

## Tension Joints

$P$  tension load per bolt

$$P = \frac{P_{\text{total}}}{N}$$

$$\frac{P_b}{K_b} = \Delta \delta_b = \Delta \delta_m = \frac{P_m}{K_m}$$

$$P_m = \frac{K_m}{K_b} P_b$$



$$P_b = \frac{K_b P}{K_b + K_m} = cP$$

$$P_m = P - P_b = (1 - c)P$$

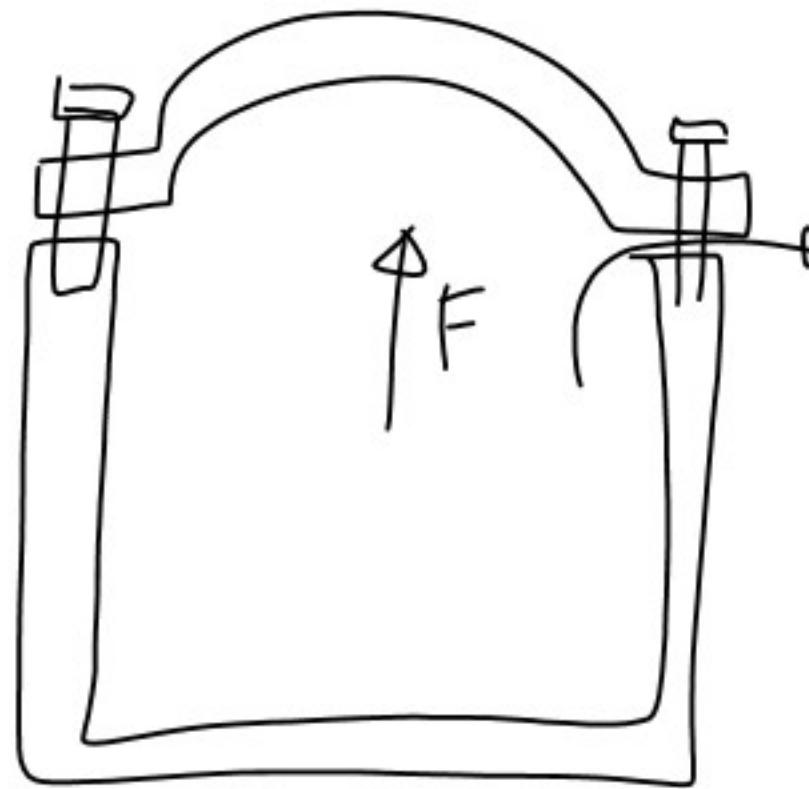
Stiffness constant

$$c = \frac{K_b}{K_b + K_m}$$

$F_i$  pre load

$$F_b = P_b + F_i = CP + \bar{F}_i$$

$$F_m = P_m - F_i = (1 - c)P - F_i$$



Torque to preload

$$T = \frac{F_i d_m}{2} \left( \frac{l + \pi f d_m \sec \alpha}{\pi d_m - f l \sec \alpha} \right) + \frac{F_i f_c d_c}{2}$$

$$T = K F_i d$$

$$K = \left( \frac{d_m}{2d} \right) \left( \frac{\tan \lambda + f \sec \alpha}{1 - f \tan \lambda \sec \alpha} \right) + 0.625 f_c$$

Table 8-15 Page 450

## Static Loading

$$\sigma_b = \frac{F_b}{A_t} = \frac{CP - F_i}{A_t}$$

$$n_p = \frac{s_p}{\sigma_b} = \frac{s_p A_t}{CP + F_i}$$

## Load Factor

$$s_p = \frac{C_{uL} P + F_i}{A_t}$$

$$n_L = \frac{s_p A_t - F_i}{CP}$$

Factor of safety on  
Separation

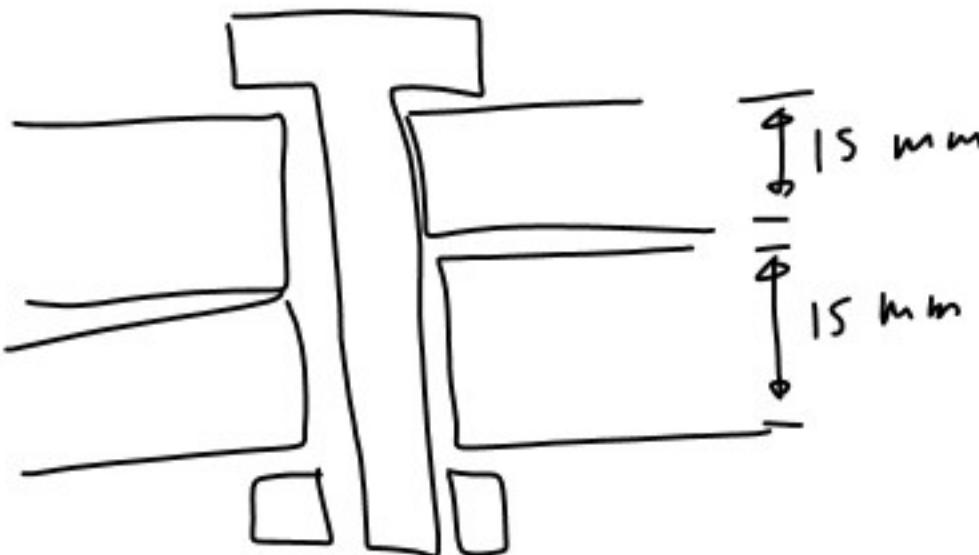
$$n_D = \frac{F_i}{P(1-C)}$$

$$F_i = \begin{cases} 0.75 F_p & \text{reused fasteners} \\ 0.95 F_p & \text{permanent bolts} \end{cases}$$

$$F_p = A_t s_p \quad \text{proof force}$$

**8-11** An M14 × 2 hex-head bolt with a nut is used to clamp together two 15-mm steel plates.

- Determine a suitable length for the bolt, rounded up to the nearest 5 mm.
- Determine the bolt stiffness.
- Determine the stiffness of the members.



$$L > l + H$$

$$L > 30 + 12.8$$

$$L > 42.8$$

$$L = 45 \text{ mm}$$

$$\phi = 15 \text{ mm} \cdot 2 = 30 \text{ mm}$$

$$H = 12.8 \text{ mm}$$

A-31

$$K_b = \frac{A_d A_t E}{A_d l_t + A_t l_d} = \frac{154 \text{ mm}^2 \cdot 115 \text{ mm} \cdot 207 \text{ GPa}}{154 \text{ mm}^2 \cdot 19 \text{ mm} + 115 \text{ mm}^2 \cdot 11 \text{ mm}} = \frac{3665170 \text{ mm}^4 \text{ GPa}}{9191 \text{ mm}^3}$$

$$= 375 \text{ MN/m}^2 \left( \frac{1 \text{ m}}{1000 \text{ mm}} \right) \left( \frac{1 \times 10^9 \text{ Pa}}{1 \text{ GPa}} \right) \left( \frac{1 \text{ N/mm}^2}{1 \text{ Pa}} \right)$$

$$A_d = \pi d^2 / 4 = \pi 14^2 / 4 = 154 \text{ mm}^2$$

$$A_t = 115 \text{ mm}^2$$

Table 8-1

$$k_b = 375 \times 10^6 \text{ N/m}$$

$$l_t = l - l_d = 30 - 11 = 19 \text{ mm}$$

$$l_d = L - l_T = 45 - (2d + 6) = 45 - (2 \cdot 14 + 6) = 11 \text{ mm}$$

$$E = 207 \text{ GPa}$$

$$A = 0.73715 \quad B = 0.62873$$

$$\frac{k_m}{E_d} = Ae^{\frac{Bd}{\lambda}}$$

$$k_m = E_d A e^{\frac{Bd}{\lambda}}$$
$$= 207 \text{ GPa} \cdot 19 \text{ mm} \cdot 0.73715 e^{\frac{0.62873 \cdot 19}{30}} = 3059 \text{ GPa mm} \left( \frac{1 \times 10^9 \text{ N/m}}{1 \text{ GPa mm}} \right) \boxed{3.059 \times 10^9 \text{ N/m}}$$

**8-29** For a bolted assembly with six bolts, the stiffness of each bolt is  $k_b = 3 \text{ Mlbf/in}$  and the stiffness of the members is  $k_m = 12 \text{ Mlbf/in}$  per bolt. An external load of 80 kips is applied to the entire joint. Assume the load is equally distributed to all the bolts. It has been determined to use  $\frac{1}{2} \text{ in-13 UNC grade 8 bolts with rolled threads}$ . Assume the bolts are preloaded to 75 percent of the proof load.

- (a) Determine the yielding factor of safety.
- (b) Determine the overload factor of safety.
- (c) Determine the factor of safety based on joint separation.

$$P_{total} = 80 \text{ kips}$$

$$P = \frac{P_{total}}{N} = \frac{80}{6} = 13.33 \text{ kips}$$

$$\sigma_p = 120 \text{ ksi} \quad F_p = \sigma_p A_t = 120 \cdot 0.1419 = 17.03 \text{ kips}$$

$$A_t = 0.1419 \text{ in}^2$$

$$\sigma_y = 130 \text{ ksi} \quad h = \frac{\sigma_y A_t}{(cP + F_i)} = \frac{130 \text{ ksi} \cdot 0.1419 \text{ in}^2}{0.2 \cdot 13.33 \text{ kips} + 12.77 \text{ kips}} \boxed{f1.2}$$

$$F_i = 0.75 F_p \\ = 0.75 \cdot 17.03 = 12.77 \text{ kips}$$

$$C = \frac{k_b}{k_b + k_m} = \frac{3}{3+12} = 0.2$$