

imp.tf Transfer functions via impedance

- Now the true power of impedance-based modeling is revealed: we can skip a time-domain model (e.g. state-space or io differential equation) and derive a transfer-function model, directly! Before we do, however, let's be sure to recall that a transfer-function model concerns itself with the forced response of a system, ignoring the free response. If we care to consider the free response, we can convert the transfer function model to an io differential equation and solve it.
- There are two primary ways impedance-based modeling is used to derive transfer functions. The first and most general is described, here. The second is a shortcut most useful for relatively simple systems; it is described in Lec. imp.divide.
- In what follows, it is important to recognize that, in the Laplace-domain, every elemental equation is just¹

$$V = \mathcal{I}Z, \quad (1)$$

where the across-variable, through-variable, and impedance are all element-specific.

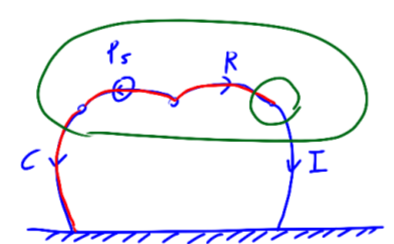
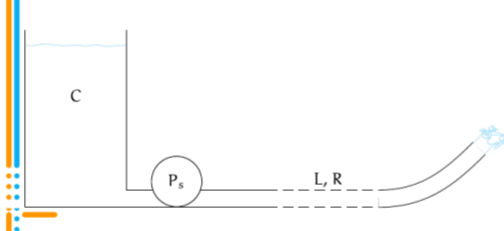
4 This algorithm is very similar to that for state-space models from linear graph models, presented in Lec. ss.nt2ss. In the following, we consider a connected graph with B branches, of which S are sources (split between through-variable sources S_T and across S_A). There are $2B - S$ unknown across- and through-variables, so that's how many equations we need. We have $B - S$ elemental equations and for the rest we will write continuity and compatibility equations. N is the number of nodes.

- Derive $2B - S$ independent Laplace-domain, algebraic equations from Laplace-domain elemental, continuity, and compatibility equations.
 - Draw a normal tree. **normal tree**
 - Write a Laplace-domain elemental equation for each passive element.² **elemental equation**
 - Write a continuity equation for each passive branch by drawing a contour intersecting that and no other branch.³ **continuity equation**
 - Write a compatibility equation for each passive link by temporarily "including" it in the tree and finding the compatibility equation for the resulting loop.⁴ **compatibility equation**
- Solve the algebraic system of $2B$ equations and $2B$ unknowns for outputs in terms of inputs, only. Sometimes, solving for all unknowns via the usual methods is easier than trying to cherry-pick the desired outputs.
- The solution for each output Y_i depends on zero or more inputs U_j . To solve for the transfer function Y_i/U_j , set $U_k = 0$ for all $k \neq j$, then divide both sides of the equation by U_j .

¹ In electronics, this is sometimes called "generalized Ohm's law."

Example imp.tf-1 re: fire hose

For the schematic of a fire hose connected to a fire truck's reservoir C via pump input P_s , use impedance methods to find the transfer function from P_s to the velocity of the spray. Assume the nozzle's cross-sectional area is A .



$$\begin{aligned} v_C &= q_C Z_C & q_R &= q_I \\ P_R &= q_R Z_R & q_C &= q_I \\ q_C &= q_I Z_I & P_I &= P_C + P_S - P_R \end{aligned}$$

$$\begin{aligned} q_I &= \frac{P_I}{Z_I} = \frac{1}{Z_I} (P_C + P_S - P_R) \\ &= \frac{1}{Z_I} (q_C Z_C + P_S - q_R Z_R) \\ q_I &= \frac{1}{Z_I} (q_I Z_C + P_S - q_I Z_R) \end{aligned}$$

$$\begin{aligned} Z_I q_I &= q_I Z_C + P_S - q_I Z_R \\ Z_I q_I - q_I Z_C + q_I Z_R &= P_S \\ q_I (Z_I + Z_R - Z_C) &= P_S \end{aligned}$$

$$q_I = \frac{P_S}{Z_I + Z_R - Z_C}$$

$$\frac{q_I}{P_S} = \frac{1}{Z_I + Z_R + Z_C}$$

$$\begin{aligned} \frac{V_h}{P_S} &= \frac{1}{A} \frac{1}{Z_I + Z_R + Z_C} \\ &= \frac{1}{A} \frac{1}{I_s + R + 1/Cs} \frac{Cs}{Cs} \\ &= \frac{1}{A} \frac{Cs}{Cs^2 + Rcs + 1} \end{aligned}$$

unknowns = $\begin{bmatrix} P_C \\ P_R \\ P_I \\ q_C \\ q_R \\ q_I \end{bmatrix}$

$$\begin{bmatrix} 1 & 0 & 0 & -Z_C & 0 & 0 \\ 0 & 0 & 0 & 0 & -1 & 1 \\ -1 & 1 & 1 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} P_C \\ P_R \\ P_I \\ q_C \\ q_R \\ q_I \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ P_S \end{bmatrix}$$

$$q_I - q_R = 0 \Rightarrow q_I = q_R$$

$$q_I = \frac{V}{l} = \frac{h^3}{s}$$

$$\frac{q_I}{A} = \frac{h^3}{s m^2} = \frac{m}{s}$$