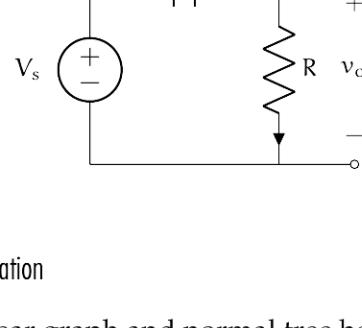


## Problem quantizer

Given the circuit below, find the steady state output voltage  $v_o$  in trigonometric form,  $v_o = B \cos(\omega t + \phi)$ , with the input voltage,  $V_s = A \cos(\omega t + \frac{\pi}{4})$ . For this problem:

- a** find the output amplitude  $B$ , and
- b** determine the output phase  $\phi$ .



\_\_\_\_/30 p.

$$Z_R = R$$

$$Z_C = \frac{1}{j\omega C}$$

$$V_o = V_s \frac{Z_R}{Z_C + Z_R} = V_s Z$$

$$Z = \frac{R}{\frac{1}{j\omega C} + R} = \frac{j\omega RC}{1 + j\omega RC} = \frac{(1 - j\omega RC)}{(1 + j\omega RC)}$$

$$= \frac{j\omega RC + \omega^2 R^2 C^2}{1 + \omega^2 R^2 C^2}$$

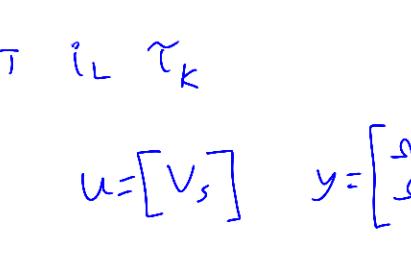
$$|Z| = \frac{\sqrt{\omega^2 R^2 C^2 + \omega^2 R^4 C^4}}{1 + \omega^2 R^2 C^2}$$

## Problem levitation

In the linear graph and normal tree below a system is depicted consisting of a motor driven by a voltage source  $V_s$  with inertia  $J$  driving a rotary damper and spring connected in series. Let the motor constant be  $K_a$ , and outputs of the system be the rotational velocity of the inertia,  $\Omega_J$ , and the change in rotational velocity across the rotational damper,  $\tau_K$ .

Given this linear graph and normal tree:

- a** determine the state variables,
- b** define the state, input, and output vectors,
- c** write the elemental, continuity, and compatibility equations, and
- d** solve for the state and output equations.



\_\_\_\_/40 p.

$$\angle(Z) = \tan^{-1}\left(\frac{\omega RC}{\omega^2 R^2 C^2}\right)$$

$$= \tan^{-1}\left(\frac{1}{\omega RC}\right)$$

$$Z = |Z| e^{\angle(Z)}$$

$$V_s = A \cos(\omega t + \frac{\pi}{4}) = A e^{\frac{\pi i}{4}}$$

$$V_o = V_s Z = A e^{\frac{\pi i}{4}} |Z| e^{\angle(Z)}$$

$$= A |Z| e^{\frac{\pi i}{4} + \angle(Z)}$$

$$B = A |Z| \boxed{B = A \frac{\omega RC \sqrt{\omega^2 R^2 C^2 + 1}}{1 + \omega^2 R^2 C^2}}$$

$$\phi = \frac{\pi}{4} + \angle(Z)$$

$$\phi = \frac{\pi}{4} + \tan^{-1}\left(\frac{1}{\omega RC}\right)$$

State  $\Omega_J$   $i_L$   $\tau_K$

$$x = \begin{bmatrix} i_L \\ \Omega_J \\ \tau_K \end{bmatrix} \quad u = [V_s] \quad y = \begin{bmatrix} \Omega_J \\ \Omega_B \end{bmatrix}$$

Primary:  $v_R$   $v_1$   $v_s$   $i_L$   $\Omega_J$   $\Omega_B$   $\tau_K$   $\tau_2$

Elemental:

$$v_R = R i_L = R i_L$$

$$\frac{d i_L}{dt} = \frac{1}{L} v_L = \frac{1}{L} (V_s - v_R - v_1) = \frac{1}{L} (V_s - R i_L - K_a \Omega_J)$$

$$\begin{bmatrix} v_1 \\ i_1 \end{bmatrix} = \begin{bmatrix} \Omega_J \\ \tau_1 \end{bmatrix} \begin{bmatrix} K_a & 0 \\ 0 & -\frac{1}{K_a} \end{bmatrix} \quad v_1 = \Omega_J K_a = K_a \Omega_J$$

$$\tau_1 = -K_a i_1 = -K_a i_L$$

$$\frac{d \Omega_J}{dt} = \frac{1}{J} \tau_J = \frac{1}{J} (-\tau_1 - \tau_K) = \frac{1}{J} (K_a i_L - K (\Omega_J - \Omega_B))$$

$$\Omega_B = \frac{1}{B} \tau_B = \frac{1}{B} \tau_K = \frac{1}{B} (K_a i_L - K (\Omega_J - \frac{1}{B} \tau_K))$$

Continuity:

$$i_R = i_L$$

$$i_1 = i_L$$

$$\tau_B = \tau_K$$

$$\tau_J = -\tau_1 - \tau_K$$

Compatibility:

$$v_L = V_s - v_R - v_1$$

$$\Omega_2 = \Omega_J$$

$$\Omega_K = \Omega_J - \Omega_B$$

$$\dot{x} = \begin{bmatrix} \frac{di_L}{dt} \\ \frac{d\Omega_J}{dt} \\ \frac{d\tau_K}{dt} \end{bmatrix}$$

$$\dot{x} = \begin{bmatrix} -R/L & -K_a/L & 0 \\ K_a/J & -K/J & K/JB \\ 0 & K & -K/B \end{bmatrix} x + \begin{bmatrix} 1/L \\ 0 \\ 0 \end{bmatrix} u$$

$$y = \begin{bmatrix} \Omega_J \\ \Omega_B \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1/B \end{bmatrix} \begin{bmatrix} i_L \\ \Omega_J \\ \tau_K \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} [V_s]$$

$$y = \begin{bmatrix} \Omega_J \\ \Omega_B \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1/B \end{bmatrix}}_C \begin{bmatrix} i_L \\ \Omega_J \\ \tau_K \end{bmatrix} + \underbrace{\begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}}_D [V_s]$$